

High-Side Measurement Current-Shunt Monitor with Comparator

General Description

The RTQ6052 devices are high-side current-shunt monitors which contain a current-sense amplifier, bandgap reference, and a comparator with latching output. The RTQ6052 senses drops across shunts at common-mode voltages from 2V to 80V. The RTQ6052 series supports 100V/V output voltage scale.

The RTQ6052 builds in an open-drain comparator and internal reference providing a 0.6V threshold. External dividers set the current trip point. The comparator features a latching capability, that can be made easily by grounding (or leaving open) the RESET pin.

The RTQ6052 is available in a small 8-pins MSOP package.

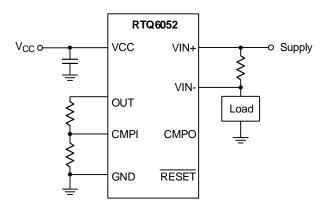
Features

- High Accuracy Current Sensing
- 3.5% Maximum Error Over Temperature
- 2.9V to 18V Power-Supply Range
- RTQ6052 Gain = 100V/V
- Common-Mode Range: 2V to 80V
- 0.6V Internal Voltage Reference
- Internal Open-Drain Comparator
- Latching Capability on Comparator
- Packages: MSOP-8

Applications

- Server, Storage and Network Equipment
- Portable, Battery-Powered Systems
- Point of Load (POL) Power Modules
- Notebook Computers
- · High End Digital TVs

Simplified Application Circuit



DSQ6052-00 April 2022 www.richtek.com



Ordering Information

RTQ605 □ □ □ Package Type F: MSOP-8 Lead Plating System G: Green (Halogen Free and Pb Free) **Gain Options** 2:100V/V

Marking Information

12=YM DNN

12=: Product Code YMDNN: Date Code

Note:

Richtek products are:

- ▶ RoHS compliant and compatible with the current requirements of IPC/JEDEC J-STD-020.
- ▶ Suitable for use in SnPb or Pb-free soldering processes.

Pin Configuration

(TOP VIEW) VIN+ □ VIN-СМРІ Г CMPO 6 RESET GND [MSOP-8

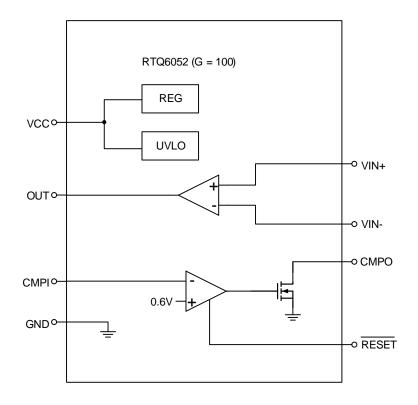
Functional Pin Description

Pin No.	Pin Name	Pin Function				
1	VCC	Power input. Connect a 0.1µF capacitor as close to the VCC pin as possible.				
2	OUT	Voltage output. Vo∪⊤ is proportional to Vsense (VIN+ – VIN-).				
3	СМРІ	Comparator input. Positive input of an internal comparator. The negative terminal is connected to a 0.6V internal reference.				
4	GND	Ground.				
5	RESET	Reset input pin. Reset the output latch of the comparator, active low.				
6	СМРО	Open-drain comparator output. Connect RESET to GND to disable the latch.				
7	VIN-	Negative current-sensing input. Connect load side to external sense resistor.				
8	VIN+	Positive current-sensing input. Connect power side to external sense resistor.				

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Functional Block Diagram



Operation

The RTQ6052 devices are high-side, unidirectional, current-shunt monitors with a high common-mode input range from 2V to 80V. The devices are available with two output voltage scales: 20V/V and 100V/V, with up to 500kHz bandwidth. The over-current protection is also available by internal comparator; when the voltage at CMPI pin is higher than internal reference 0.6V, the CMPO pulls high to indicate over-current situation. Connect a divider from the OUT pin to CMPI pin to set the over-current trip point, the devices provide an opendrain comparator with a latching function that allow the output signal of comparator to be latched or non-latched by RESET pin setting.

Comparator and Reset

The RTQ6052 devices incorporate an open-drain comparator. This comparator typically has $1.3\mu s$ (typical) response time. The output of the comparator latches and is reset through the \overline{RESET} pin. From Figure 1, the control logic can be described as 3 stages.

Stage1. VCMPO goes high after VCMPI increases and eventually over 0.6V.

Stage2. When VRESET is high, VCMPO is kept high even VCMPI decreases and lower than 0.6V; when VRESET goes low, VCMPO goes low as well.

Stage3. When VRESET is low, VCMPO goes high/low depending on VCMPI higher/lower than 0.6V.

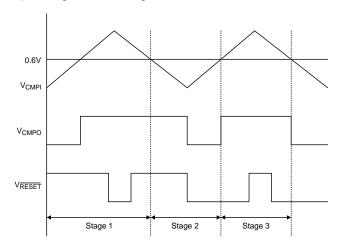


Figure 1. Comparator Latching and Reset Logic

Power-On

The RTQ6052 implements power-on reset (POR) function to prevent operation without fully turn-on the

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internal control circuit. When Vcc is increasing and eventually becomes higher than POR rising threshold (2.75V, typical), the device starts output voltage; in contrast, when Vcc is lower than POR falling threshold (2.55V, typical), the device stops output voltage.

Gain Error and Input Offset Voltage

Using two-step method to characterize gain error and offset voltage, first of all, the gain can be obtained by measuring different sense voltage.

$$G = \frac{V_{OUT1} - V_{OUT2}}{100mV - 20mV}$$

Where

- Vout1 = output voltage with Vsense = 100mV
- Vout2 = output voltage with Vsense = 20 V

Then the offset voltage is measured at VSENSE = 100mV, and referred to the input (RTI) of the current shunt monitor, as shown in Electrical Characteristics: Current-Shunt Monitor section.

$$VRTI \ \left(Referred\text{-}To\text{-}Input\right) = \left(\frac{V_{OUT1}}{G}\right) - 100 mV$$



Absolute Maximum Ratings (Note 1)

• Supply Input Voltage, Vcc	0.3V to 19.8V
Power Sensing PINS, VIN+, VIN- (common mode), VCM	6V to 88V
Power Sensing PINS, VIN+ -VIN- (different mode), VSENSE	6V to 18V
Other Pins, CMPI, CMPO, OUT, RESET	0.3V to 19.8V
 Power Dissipation, PD @ TA = 25°C 	
MSOP-8	- 0.27W
Package Thermal Resistance (Note 2)	
MSOP-8, θJA	- 361.6°C/W
MSOP-8, θJC	- 90.4°C/W
Lead Temperature (Soldering, 10 sec.)	- 260°C
• Junction Temperature	- 150°C
Storage Temperature Range	65°C to 150°C
• ESD Susceptibility (Note 3)	
HBM (Human Body Model)	- 4kV
Recommended Operating Conditions (Note 4)	
Supply Input Voltage, Vcc	- 2.9V to 18V
Common mode input range, Vcм	- 2V to 80V
Ambient Temperature Range	- −40°C to 85°C

Electrical Characteristics

(V_{CC} = 12V, V_{CM} = 12V, T_A = 25°C, unless otherwise specified)

Parameter	Symbol	Test Conditions	Min	Тур	Max	Unit				
Power Supply										
Operating Power Supply	Vcc		2.9		18	V				
0		Vout = 2V, Ta = -40°C to 125°C			1200					
Quiescent Current	lQ	VSENSE = 0mV, TA = -40°C to 125°C			500	μΑ				
POR Rising Threshold	Vporh		2.7	2.75	2.85	V				
POR Falling Threshold	VPORL			2.55		V				
Current Sense	Current Sense									
Full Scale Sense Input Voltage				0.15		V				
Common Mode Input Range	Vсм		2		80	V				
Common Mode Rejection (Note 5)		V _{IN+} = 2V to 80V	80	100		dB				
	CMR	V _{IN+} = 12V to 80V T _A = -40°C to125°C	100	123		dB				

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Parameter	Symbol	Test Conditions	Min	Тур	Max	Unit
Offeet Voltage PTI	Vos	T _A = 25°C		±0.5	±2.5	mV
Offset Voltage, RTI	VUS	T _A = -40°C to 125°C		±3.5		mV
Offset Voltage. RTI vs Temperature (Note 5)		T _A = -40°C to 125°C 5				μV/°C
PSR of Offset Voltage, RTI	PSR	V _{OUT} = 2V, V _{IN+} = 18V, V _{CC} = 2.9V T _A = -40°C to 125°C	100	μV/V		
Input bias current	lв	VIN- pin		μΑ		
Gain	G			100		V/V
		VSENSE = 20mV to 100mV		±0.2	±1	%
Gain Error	GE%	VSENSE = 20mV to 100mV TA = -40°C to 125°C			±2	%
		Vsense = 120mV, Vcc = 16V		±0.75	±2.2	%
Total Output Error	∆Vout%	VSENSE = 120mV, VCC = 16V TA = -40°C to 125°C			±3.5	%
Nonlinearity Error (Note 5)	NLIN%	VSENSE = 20mV to 100mV		0.1		%
Maximum Capacitive Load (Note 5)				10		nF
Output Voltage Range H		V _{IN-} =11V, V _{IN+} = 12V T _A = -40°C to 125°C		Vcc -0.15		V
Output Voltage Range L		V _{IN} -= 0V, V _{IN} + = -0.5V T _A = -40°C to 125°C		4	350	mV
Bandwidth (Note 5)	BW	GAIN = 100, CLOAD = 5pF, unity gain		36		kHz
Phase Margin (Note 5)	P.M	CLOAD < 10nF		40		0
Slew Rate	SR			1.5		V/μs
Settling Time	Tst	Vsense = 10mV to 100mV 10%~90% Vout, CLOAD = 5pF		6		μs
Noise Density, RTI (Note 5)		Frequency = 10k		40		nV/√Hz
Comparator						
Threshold	Vтн	T _A = -40°C to 125°C		600	615	mV
Hysteresis	V _H YS	T _A = -40°C to 85°C		-8		mV
January Diago Occupant	Ів_см	TA = 25°C		0.005	10	nA
Input Bias Current		T _A = -40°C to 125°C			15	nA
Maximum Input				Vcc -1.5		V
Output Open-Drain						
Voltage Gain (Note 5)	CMPGAIN			200		V/mV
Leakage Current	ILEAK			0.0001	1	μΑ
Dropout Voltage	VDROP	ILOAD = 2.35mA			220	mV



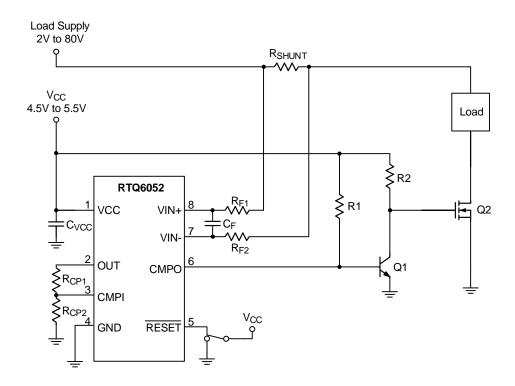
Parameter	Symbol	Test Conditions	Min	Тур	Max	Unit
Response Time	TRS	R _L to 5V, C _L = 15pF 100mV input step with 10mV overdrive		1.3		μS
RESET						
DECET Die Theorie	VRST_H	High Level	1			V
RESET Pin Threshold	VRST_L	Low Level			0.4	V
RESET Input Impedance				2		MΩ
RESET Minimum Pulse Width			1	1.5	1	μS
RESET Propagation Delay				1.6		μS

- Note 1. Stresses beyond those listed under "Absolute Maximum Ratings" may cause permanent damage to the device. These are stress ratings only, and functional operation of the device at these or any other conditions beyond those indicated in the operational sections of the specifications is not implied. Exposure to absolute maximum rating conditions may affect device reliability.
- Note 2. θ_{JA} is measured under natural convection (still air) at T_A = 25°C with the component mounted on a high effective-thermalconductivity four-layer test board on a JEDEC 51-7 thermal measurement standard.
- Note 3. Devices are ESD sensitive. Handling precautions are recommended.
- **Note 4.** The device is not guaranteed to function outside its operating conditions.
- Note 5. Specifications are guaranteed by design, not production tested.

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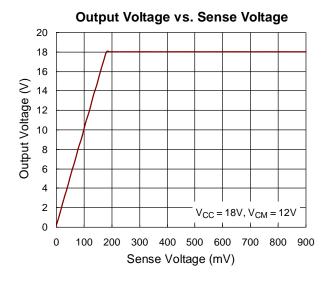


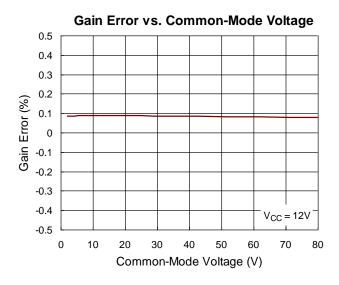
Typical Application Circuit

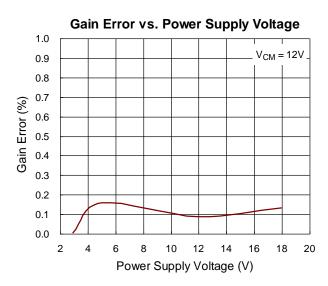


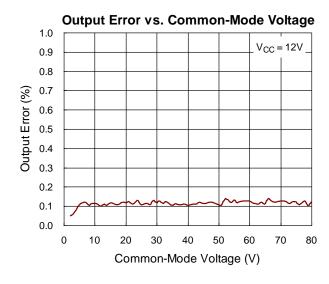


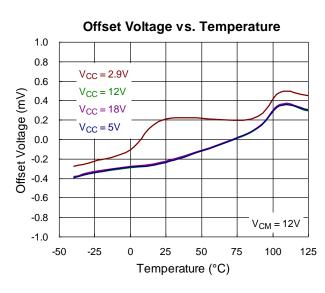
Typical Operating Characteristics

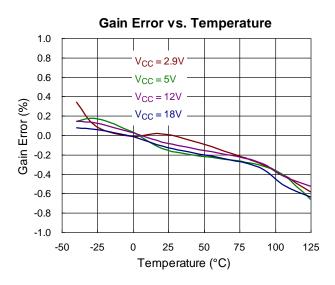








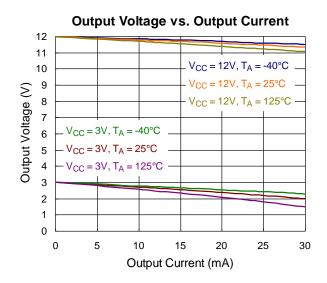


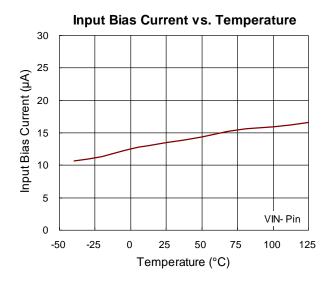


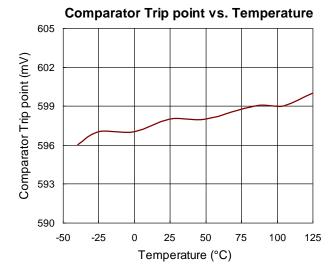
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Application Information

Selecting the Shunt Resistor

The selected value for the shunt resistor, RSHUNT, depends on the application and is a compromise between small-signal accuracy and maximum permissible voltage loss in the measurement line. High values of RSHUNT provide better accuracy at lower currents by minimizing the effects of offset, while low values of RSHUNT minimize voltage loss in the supply line. For best performance, select RSHUNT to provide approximately 50mV to 100mV of sense voltage for the full-scale current in each application. Maximum input voltage for accurate measurements is 500mV, but output voltage is limited by supply voltage Vcc.

Input Filtering

In some applications, the current being measured may be inherently noisy. In the case of a noisy signal, filtering after the output of the current sense amplifier is often simpler; however, this location negates the advantage of the low output impedance of the internal buffer.

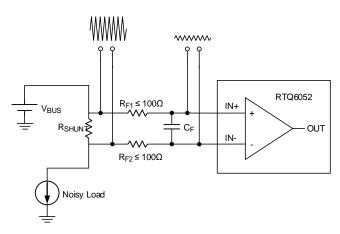


Figure 2. Input Filter

Other applications may require filtering at the input of the current sense amplifier. Figure 2 shows the recommended schematic for input filtering.

Input filtering is complicated by the fact that the mismatch between added resistance of the filter resistors and the associated resistance can adversely affect gain, CMR, and offset voltage, Vos. The effect on Vos is partly due to input bias currents as well. As a result, the value of the input resistors should be limited to 100Ω or less.

Total Error Analysis

To optimize the design, the first is to analyze each error contributed; the main influences of sense voltage errors can be identified as follows:

- The tolerance of shunt resistor (RSHUNT)
- Sense offset voltage, Vos. When the sense voltage is small, especially low load current and small shunt resistance, the error is dominated by the input offset error.
- Gain Error, GE%
- PSR of offset voltage, PSR
- Common mode rejection, CMR
- The offset voltage caused by input bias current
- Nonlinearity Error, NLIN%

Max Output Error Estimation

Here is an example. The system bus voltage V_{CM_SYS} connects to VIN+ = 18V, system supply voltage V_{CC_SYS} = 12V, shunt resistor accuracy is 1%, 10m Ω 1.5W, the load current is 10A. To set the design goals, the maximum output voltage errors are calculated in the following sections.

Input Offset Voltage Error

The rate of offset error in the total error can be estimated directly from the specification table. The input offset voltage is 2.5mV at $T_A = 25^{\circ}\text{C}$; the error due to offset can be obtained by the equation below :

$$V_{OS_err} = \frac{V_{OS(max)}}{V_{SENSE}} \times 100\% = \frac{2.5mV}{10m\Omega \times 10A} \times 100\% = 2.5\%$$

Shunt Voltage Gain Error

From the electrical characteristics, the max gain error is 1%.

PSR Error

The PSR error is to estimate the error caused by different supply voltages. The RTQ6052 device specification gives the specified power supply voltage for the input offset voltage specification as VCC_DS = 2.9V; when the system supply voltage is not exactly 2.9V, it may result in an additional error. RTQ6052

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device gives the maximum PSR as 50µV/V. Calculate the PSR error by the equation below:

$$PSR_err = \frac{\left|V_{CC_DS} - V_{CC_SYS}\right| \times PSR}{V_{SENSE}} \times 100\%$$
$$= \frac{\left|2.9 - 12V\right| \times 50 \frac{\mu V}{V}}{10mO \times 10A} \times 100\% = 0.45\%$$

CMR Error

The CMR error means the input offset error is influenced by the variation of common-mode voltage. In real conditions, calculate the maximum input offset by determining the actual common-mode voltage as applied to RTQ6052. According to the RTQ6052 device specification, it gives the common-mode rejection ratio minimum as 80dB ($100\mu V/V$). The offset voltage in the data sheet is specified with a common-mode voltage, VCM DS, that is 12V. To calculate the actual commonmode error at system bus voltage:

$$80dB = \frac{1}{10^{\left(\frac{80dB}{20}\right)}} \times 10^{6} \times \frac{\mu V}{V} = 100 \frac{\mu V}{V}$$

CMR_err =
$$\frac{\left|V_{CM_DS} - V_{CM_SYS}\right| \times CMR}{V_{SENSE}} \times 100\%$$
$$= \frac{\left|12 - 18\right| \times 100 \frac{\mu V}{V}}{10 M C \times 10A} \times 100\% = 0.6\%$$

Input Bias Current Error

The input bias current flows into shunt resistor to cause additional offset; this error is calculated with respect to the ideal voltage across the sense voltage.

$$I_{B_err} = \frac{I_{B} \times R_{SHUNT}}{V_{SENSE}} \times 100\% = \frac{13\mu A \times 10m\Omega}{10m\Omega \times 10A} \times 100\%$$
$$= 0.00013\%$$

Nonlinearity Error

The nonlinearity error shown in Figure 3 is the difference between an actual gain and the ideal value. For ideal cases, the voltage gain is constant over full sense ranges, but in the real application, the voltage gain is not exactly constant, and the nonlinearity gain may cause additional errors. In the specification, the RTQ6052 gives the nonlinearity error as 0.1% over sense voltage from 20mV to 100mV.

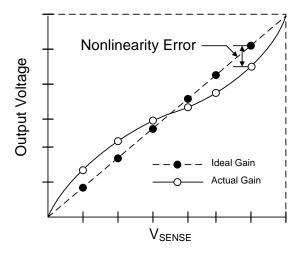


Figure 3. Nonlinearity Error

Total Error

Use equation below to calculate the worst case of total error:

Total_err =
$$\sqrt{(GE\%)^2 + (R\%)^2 + (V_{OS_err})^2 + (PSR_err)^2 + (CMR_err)^2 + (I_{B_err})^2 + (NLIN\%)^2}$$

= $\sqrt{(1\%)^2 + (1\%)^2 + (2.5\%)^2 + (0.45\%)^2 + (0.6\%)^2 + (0.0013\%)^2 + (0.1\%)^2}$
= 3.07%



Layout Guidelines

- ▶ A Kelvin sense arrangement is required for best performance. Connect the input pins (VIN+ and VIN-) to the sensing resistor using a 4-wire connection.
- ▶ PCB trace resistance from the sense resistor to the VIN+ and VIN- pins can affect the power measurement accuracy. Place the sense resistors as close as possible to the RTQ6052 and do not use minimum width PCB traces.
- ▶ Place the power-supply bypass capacitor 0.1μF as close as possible to the supply and ground pins.

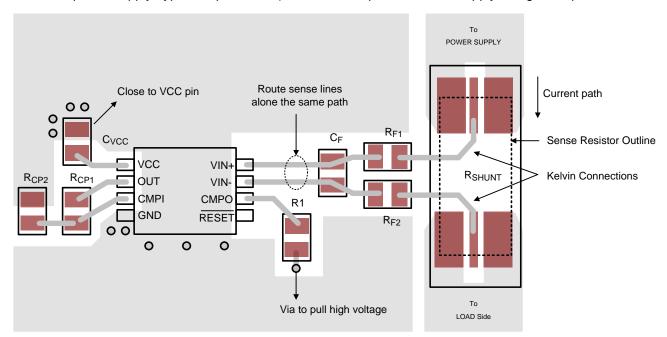
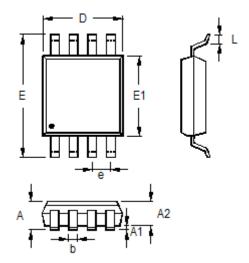


Figure 4. PCB Layout Guide



Outline Dimension

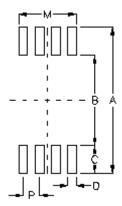


Cymah al	Dimensions I	n Millimeters	Dimensions In Inches		
Symbol	Min	Max	Min	Max	
А	0.810	1.100	0.032	0.043	
A1	0.000	0.150	0.000	0.006	
A2	0.750	0.950	0.030	0.037	
b	0.220	0.380	0.009	0.015	
D	2.900	3.100	0.114	0.122	
е	0.6	650	0.0)26	
Е	4.800	5.000	0.189	0.197	
E1	2.900	3.100	0.114	0.122	
L	0.400	0.800	0.016	0.031	

8-Lead MSOP Plastic Package



Footprint Information



Dookogo	Number of	Footprint Dimension (mm)					Toloropoo	
Package	Pin	Р	Α	В	С	D	М	Tolerance
MSOP-8	8	0.65	5.80	3.60	1.10	0.35	2.30	±0.10

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