## MAX828, MAX829

## Switched Capacitor Voltage Converter

The MAX828 and MAX829 are CMOS charge pump voltage inverters that are designed for operation over an input voltage range of 1.15 V to 5.5 V with an output current capability in excess of 50 mA . The operating current consumption is only $68 \mu \mathrm{~A}$ for the MAX828 and $118 \mu \mathrm{~A}$ for the MAX829. The devices contain an internal oscillator that operates at 12 kHz for the MAX828 and 35 kHz for the MAX829. The oscillator drives four low resistance MOSFET switches, yielding a low output resistance of $26 \Omega$ and a voltage conversion efficiency of $99.9 \%$. These devices require only two external capacitors, $10 \mu \mathrm{~F}$ for the MAX828 and $3.3 \mu \mathrm{~F}$ for the MAX829, for a complete inverter making it an ideal solution for numerous battery powered and board level applications. The MAX828 and MAX829 are available in the TSOP-5 package.

## Features

- Operating Voltage Range of 1.15 V to 5.5 V
- Output Current Capability in Excess of 50 mA
- Low Current Consumption of $68 \mu \mathrm{~A}$ (MAX828) or $118 \mu \mathrm{~A}$ (MAX829)
- Operation at 12 kHz (MAX828) or 35 kHz (MAX829)
- Low Output Resistance of $26 \Omega$
- Space Saving TSOP-5 Package
- Pb-Free Packages are Available


## Typical Applications

- LCD Panel Bias
- Cellular Telephones
- Pagers
- Personal Digital Assistants
- Electronic Games
- Digital Cameras
- Camcorders
- Hand-Held Instruments


This device contains 77 active transistors.
Figure 1. Typical Application

ON Semiconductor ${ }^{\circledR}$
http://onsemi.com


MARKING DIAGRAM


| EAx $=$ | Device Code |
| ---: | :--- |
|  | X A A or B |
| A | $=$ Assembly Location |
| Y | $=$ Year |
| W | $=$ Work Week |
| U | $=$ Pb-Free Package |

(Note: Microdot may be in either location)

PIN CONFIGURATION


ORDERING INFORMATION

| Device | Package | Shipping $^{\dagger}$ |
| :--- | :---: | :---: |
| MAX828EUK | TSOP-5 | 3000 Tape/Reel |
| MAX828EUKG | TSOP-5 <br> (Pb-Free) | 3000 Tape/Reel |
| MAX829EUK | TSOP-5 | 3000 Tape/Reel |
| MAX829EUKG | TSOP-5 <br> (Pb-Free) | 3000 Tape/Reel |

$\dagger$ For information on tape and reel specifications, including part orientation and tape sizes, please refer to our Tape and Reel Packaging Specifications Brochure, BRD8011/D.

MAXIMUM RATINGS*

| Rating | Symbol | Value | Unit |
| :---: | :---: | :---: | :---: |
| Input Voltage Range ( $\mathrm{V}_{\text {in }}$ to GND) | $V_{\text {in }}$ | -0.3 to 6.0 | V |
| Output Voltage Range (V $\mathrm{V}_{\text {out }}$ to GND) | $V_{\text {out }}$ | -6.0 to 0.3 | V |
| Output Current (Note 1) | $\mathrm{I}_{\text {out }}$ | 100 | mA |
| Output Short Circuit Duration (V ${ }_{\text {out }}$ to GND, Note 1) | tsc | Indefinite | sec |
| Operating Junction Temperature | TJ | 150 | ${ }^{\circ} \mathrm{C}$ |
| Power Dissipation and Thermal Characteristics Thermal Resistance, Junction to Air Maximum Power Dissipation @ $\mathrm{T}_{\mathrm{A}}=70^{\circ} \mathrm{C}$ | $\begin{gathered} \mathrm{R}_{\text {QJA }} \\ \mathrm{P}_{\mathrm{D}} \end{gathered}$ | $\begin{aligned} & 256 \\ & 313 \end{aligned}$ | $\begin{aligned} & { }^{\circ} \mathrm{C} / \mathrm{W} \\ & \mathrm{~mW} \end{aligned}$ |
| Storage Temperature | $\mathrm{T}_{\text {stg }}$ | -55 to 150 | ${ }^{\circ} \mathrm{C}$ |

Maximum ratings are those values beyond which device damage can occur. Maximum ratings applied to the device are individual stress limit values (not normal operating conditions) and are not valid simultaneously. If these limits are exceeded, device functional operation is not implied, damage may occur and reliability may be affected.
*ESD Ratings
ESD Machine Model Protection up to 200 V, Class B
ESD Human Body Model Protection up to 2000 V, Class 2

ELECTRICAL CHARACTERISTICS $\left(\mathrm{V}_{\text {in }}=5.0 \mathrm{~V}\right.$ for MAX828 $\mathrm{C}_{1}=\mathrm{C}_{2}=10 \mu \mathrm{~F}$, for MAX829 $\mathrm{C}_{1}=\mathrm{C}_{2}=3.3 \mu \mathrm{~F}, \mathrm{~T}_{\mathrm{A}}=-40^{\circ} \mathrm{C}$ to $85^{\circ} \mathrm{C}$, typical values shown are for $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ unless otherwise noted. See Figure 20 for test setup.)

| Characteristic | Symbol | Min | Typ | Max | Unit |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Operating Supply Voltage Range ( $\mathrm{R}_{\mathrm{L}}=10 \mathrm{k}$ ) | $V_{\text {in }}$ | 1.5 to 5.5 | 1.15 to 6.0 | - | V |
| ```Supply Current Device Operating ( \(\mathrm{R}_{\mathrm{L}}=\infty\) ) \(\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}\) MAX828 MAX829 \(\mathrm{T}_{\mathrm{A}}=85^{\circ} \mathrm{C}\) MAX828 MAX829``` | $1{ }_{\text {in }}$ |  | $\begin{gathered} 68 \\ 118 \\ \\ 73 \\ 128 \end{gathered}$ | $\begin{gathered} 90 \\ 200 \\ \\ 100 \\ 200 \end{gathered}$ | $\mu \mathrm{A}$ |
| Oscillator Frequency $\begin{gathered} \mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C} \\ \text { MAX828 } \\ \text { MAX829 } \end{gathered}$ $\begin{aligned} & \mathrm{T}_{\mathrm{A}}=-40^{\circ} \mathrm{C} \text { to } 85^{\circ} \mathrm{C} \\ & \text { MAX828 } \\ & \text { MAX829 } \end{aligned}$ | fosc | $\begin{gathered} 8.4 \\ 24.5 \\ \\ 6.0 \\ 19 \end{gathered}$ | $\begin{aligned} & 12 \\ & 35 \\ & - \end{aligned}$ | $\begin{gathered} 15.6 \\ 45.6 \\ 21 \\ 54 \end{gathered}$ | kHz |
| $\begin{aligned} & \text { Output Resistance ( } \mathrm{I}_{\text {out }}=25 \mathrm{~mA} \text {, Note } 2 \text { ) } \\ & \text { MAX828 } \\ & \text { MAX829 } \end{aligned}$ | $\mathrm{R}_{\text {out }}$ | - | $\begin{aligned} & 26 \\ & 26 \end{aligned}$ | $\begin{aligned} & 50 \\ & 50 \end{aligned}$ | $\Omega$ |
| Voltage Conversion Efficiency ( $\mathrm{R}_{\mathrm{L}}=\infty$ ) | $\mathrm{V}_{\text {EFF }}$ | 99 | 99.9 | - | \% |
| Power Conversion Efficiency ( $\mathrm{R}_{\mathrm{L}}=1.0 \mathrm{k}$ ) | P EfF | - | 96 | - | \% |

1. Maximum Package power dissipation limits must be observed to ensure that the maximum junction temperature is not exceeded.
$T_{J}=T_{A}+\left(P_{D} R_{\theta J A}\right)$
2. Capacitors $\mathrm{C}_{1}$ and $\mathrm{C}_{2}$ contribution is approximately $20 \%$ of the total output resistance.


Figure 2. Output Resistance vs. Supply Voltage MAX828


Figure 4. Output Resistance vs. Ambient Temperature MAX828


Figure 6. Output Current vs. Capacitance MAX828


Figure 3. Output Resistance vs. Supply Voltage MAX829


Figure 5. Output Resistance vs. Ambient Temperature MAX829


Figure 7. Output Current vs. Capacitance MAX829


Figure 8. Output Voltage Ripple vs. Capacitance MAX828


Figure 10. Supply Current vs. Supply Voltage MAX828


Figure 12. Oscillator Frequency vs. Ambient Temperature MAX828


Figure 9. Output Voltage Ripple vs. Capacitance MAX829


Figure 11. Supply Current vs. Supply Voltage MAX829

$\mathrm{T}_{\mathrm{A}}$, AMBIENT TEMPERATURE ( ${ }^{\circ} \mathrm{C}$ )
Figure 13. Oscillator Frequency vs. Ambient Temperature MAX829


Figure 14. Output Voltage vs. Output Current MAX828


Figure 16. Power Conversion Efficiency vs. Output Current MAX828
OUTPUT VOLTAGE RIPPLE \& NOISE $=10 \mathrm{mV} /$ Div .


TIME $=25 \mu \mathrm{~s} / \mathrm{div}$
Figure 18. Output Voltage Ripple and Noise
MAX828
 AC COUPLED
AC COUPLED


Figure 15. Output Voltage vs. Output Current MAX829


Figure 17. Power Conversion Efficiency vs. Output Current MAX829


TIME $=10 \mu \mathrm{~s} / \mathrm{div}$
Figure 19. Output Voltage Ripple and Noise MAX829


Figure 20. Test Setup/Voltage Inverter

## DETAILED OPERATING DESCRIPTION

The MAX828/829 charge pump converters inverts the voltage applied to the $\mathrm{V}_{\text {in }}$ pin. Conversion consists of a two-phase operation (Figure 21). During the first phase, switches $S_{2}$ and $S_{4}$ are open and $S_{1}$ and $S_{3}$ are closed. During this time, $\mathrm{C}_{1}$ charges to the voltage on $\mathrm{V}_{\text {in }}$ and load current is supplied from $C_{2}$. During the second phase, $S_{2}$ and $S_{4}$ are closed, and $S_{1}$ and $S_{3}$ are open. This action connects $C_{1}$ across $\mathrm{C}_{2}$, restoring charge to $\mathrm{C}_{2}$.


Figure 21. Ideal Switched Capacitor Charge Pump

## APPLICATIONS INFORMATION

## Output Voltage Considerations

The MAX828/829 performs voltage conversion but does not provide regulation. The output voltage will drop in a linear manner with respect to load current. The value of this equivalent output resistance is approximately $26 \Omega$ nominal at $25^{\circ} \mathrm{C}$ and $\mathrm{V}_{\text {in }}=5.0 \mathrm{~V}$. $\mathrm{V}_{\text {out }}$ is approximately -5.0 V at light loads, and drops according to the equation below:

$$
\begin{gathered}
V_{\text {DROP }}=I_{\text {out }} \times R_{\text {out }} \\
V_{\text {out }}=-\left(V_{\text {in }}-V_{\text {DROP }}\right)
\end{gathered}
$$

## Charge Pump Efficiency

The overall power efficiency of the charge pump is affected by four factors:

1. Losses from power consumed by the internal oscillator, switch drive, etc. (which vary with input voltage, temperature and oscillator frequency).
2. I ${ }^{2}$ R losses due to the on-resistance of the MOSFET switches on-board the charge pump.
3. Charge pump capacitor losses due to Equivalent Series Resistance (ESR).
4. Losses that occur during charge transfer from the commutation capacitor to the output capacitor when a voltage difference between the two capacitors exists.
Most of the conversion losses are due to factors 2, 3 and 4. These losses are given by Equation 1.

$$
\begin{gather*}
\mathrm{P}_{\text {LOSS }(2,3,4)}=\mathrm{I}_{\text {out }}^{2} \times \mathrm{R}_{\text {out }} \cong \mathrm{I}_{\text {out }}^{2} \times \\
{\left[\frac{1}{\left(\mathrm{f}_{\mathrm{OSC}}\right) \mathrm{C}_{1}}+8 \mathrm{R}_{\text {SWITCH }}+4 \mathrm{ESR}_{\mathrm{C}_{1}}+\mathrm{ESR}_{\mathrm{C}_{2}}\right]} \tag{eq.1}
\end{gather*}
$$

The $1 /\left(\mathrm{f}_{\text {OSC }}\right)\left(\mathrm{C}_{1}\right)$ term in Equation 1 is the effective output resistance of an ideal switched capacitor circuit (Figures 22 and 23).
The losses due to charge transfer above are also shown in Equation 2. The output voltage ripple is given by Equation 3.

$$
\begin{align*}
P_{\text {LOSS }} & =\left[0.5 C_{1}\left(\mathrm{~V}_{\text {in }}^{2}-\mathrm{V}_{\text {out }}{ }^{2}\right)\right. \\
& \left.+0.5 \mathrm{C}_{2}\left(\mathrm{~V}_{\text {RIPPLE }}{ }^{2}-2 \mathrm{~V}_{\text {out }} \mathrm{V}_{\text {RIPPLE }}\right)\right] \times \mathrm{f}_{\text {OSC }} \tag{eq.2}
\end{align*}
$$

$\mathrm{V}_{\text {RIPPLE }}=\frac{\mathrm{I}_{\text {out }}}{\left(\mathrm{f}_{\mathrm{OSC}}\right)\left(\mathrm{C}_{2}\right)}+2\left(\mathrm{I}_{\text {out }}\right)\left(\mathrm{ESR}_{\mathrm{C}_{2}}\right)$


Figure 22. Ideal Switched Capacitor Model


Figure 23. Equivalent Output Resistance

## Capacitor Selection

In order to maintain the lowest output resistance and output ripple voltage, it is recommended that low ESR capacitors be used. Additionally, larger values of $\mathrm{C}_{1}$ will lower the output resistance and larger values of $C_{2}$ will reduce output voltage ripple. (See Equation 3).

Table 1 shows various values of $\mathrm{C}_{1}, \mathrm{C}_{2}$ and $\mathrm{C}_{3}$ with the corresponding output resistance values at $25^{\circ} \mathrm{C}$. Table 2 shows the output voltage ripple for various values of $\mathrm{C}_{1}, \mathrm{C}_{2}$ and $C_{3}$. The data in Tables 1 and 2 was measured not calculated.

Table 1. Output Resistance vs. Capacitance $\left(C_{1}=C_{2}=C_{3}\right), V_{\text {in }}=4.75 \mathrm{~V}$ and $\mathrm{V}_{\text {out }}=-4.0 \mathrm{~V}$

| $\mathbf{C}_{\mathbf{1}}=\mathbf{C}_{\mathbf{2}}=\mathbf{C}_{\mathbf{3}}$ | $\mathbf{M A X 8 2 8} \mathbf{R}_{\text {out }}$ <br> $(\boldsymbol{\Omega})$ | MAX829 $\mathbf{R}_{\text {out }}$ <br> $(\boldsymbol{\Omega})$ |
| :---: | :---: | :---: |
| 0.7 | 127.2 | 55.7 |
| 1.4 | 67.7 | 36.8 |
| 3.3 | 36 | 26.0 |
| 7.3 | 26.7 | 24.9 |
| 10 | 25.9 | 25.1 |
| 24 | 24.3 | 25.2 |
| 50 | 24 | 24 |

Table 2. Output Voltage Ripple vs. Capacitance $\left(C_{1}=C_{2}=C_{3}\right), V_{\text {in }}=4.75 \mathrm{~V}$ and $\mathrm{V}_{\text {out }}=-4.0 \mathrm{~V}$

| $\mathbf{C}_{\mathbf{1}}=\mathbf{C}_{\mathbf{2}}=\mathbf{C}_{\mathbf{3}}$ <br> $\mathbf{( \mathbf { F } )} \mathbf{~}$ | MAX828 Ripple <br> $(\mathbf{m V})$ | MAX829 Ripple <br> $(\mathbf{m V})$ |
| :---: | :---: | :---: |
| 0.7 | 377.5 | 320 |
| 1.4 | 360.5 | 234 |
| 3.3 | 262 | 121 |
| 7.3 | 155 | 62.1 |
| 10 | 126 | 51.25 |
| 24 | 55.1 | 25.2 |
| 50 | 36.6 | 27.85 |

## Input Supply Bypassing

The input voltage, $\mathrm{V}_{\text {in }}$ should be capacitively bypassed to reduce AC impedance and minimize noise effects due to the switching internals in the device. If the device is loaded from $V_{\text {out }}$ to GND, it is recommended that a large value capacitor (at least equal to $\mathrm{C}_{1}$ ) be connected from $\mathrm{V}_{\text {in }}$ to GND. If the device is loaded from $V_{\text {in }}$ to $V_{\text {out }}$ a small $(0.7 \mu \mathrm{~F})$ capacitor between the pins is sufficient.

## Voltage Inverter

The most common application for a charge pump is the voltage inverter (Figure 20). This application uses two or three external capacitors. The capacitors $\mathrm{C}_{1}$ (pump capacitor) and $C_{2}$ (output capacitor) are required. The input bypass capacitor $\mathrm{C}_{3}$, may be necessary depending on the application. The output is equal to $-\mathrm{V}_{\text {in }}$ plus any voltage drops due to loading. Refer to Tables 1 and 2 for capacitor selection. The test setup used for the majority of the characterization is shown in Figure 20.

## Layout Considerations

As with any switching power supply circuit, good layout practice is recommended. Mount components as close together as possible to minimize stray inductance and capacitance. Also use a large ground plane to minimize noise leakage into other circuitry.

## Capacitor Resources

Selecting the proper type of capacitor can reduce switching loss. Low ESR capacitors are recommended. The MAX828 and MAX829 were characterized using the capacitors listed in Table 3. This list identifies low ESR capacitors for the voltage inverter application.

Table 3. Capacitor Types

| Manufacturer/Contact | Part Types/Series |
| :--- | :---: |
| AVX | TPS |
| 843-448-9411 |  |
| www.avxcorp.com | ESRD |
| Cornell Dubilier |  |
| 508-996-8561 |  |
| www.cornell-dubilier.com |  |
| Sanyo/Os-con | SN |
| 619-661-6835 |  |
| www.sanyovideo.com/oscon.htm |  |
| Vishay | 593 D |
| 603-224-1961 |  |
| www.vishay.com | 594 |



Figure 24. Voltage Inverter

## MAX828, MAX829

The MAX828 / 829 primary function is a voltage inverter. The device will convert 5.0 V into -5.0 V with light loads. Two capacitors are required for the inverter to function. A third capacitor, the input bypass capacitor, may be required depending on the power source for the inverter. The performance for this device is illustrated below.


Figure 25. Voltage Inverter Load Regulation Output Voltage vs. Output Current MAX828


Figure 26. Voltage Inverter Load Regulation Output Voltage vs. Output Current MAX829


Figure 27. Cascade Devices for Increased Negative Output Voltage

Two or more devices can be cascaded for increased output voltage. Under light load conditions, the output voltage is approximately equal to $-\mathrm{V}_{\text {in }}$ times the number of stages. The converter output resistance increases dramatically with each additional stage. This is due to a reduction of input voltage to each successive stage as the converter output is loaded. Note that the ground connection for each successive stage must connect to the negative output of the previous stage. The performance characteristics for a converter consisting of two cascaded devices are shown below.


Figure 28. Cascade Load Regulation, Output Voltage vs. Output Current MAX828


Figure 29. Cascade Load Regulation, Output Voltage vs. Output Current MAX829

| Curve | $\mathrm{V}_{\text {in }}(\mathrm{V})$ | $\mathbf{R}_{\text {out }}(\boldsymbol{\Omega})$ |
| :---: | :---: | :---: |
| A | 3.0 | 173 |
| B | 5.0 | 141 |
| C | 3.0 | 179 |
| D | 5.0 | 147 |



Figure 30. Negative Output Voltage Doubler

A single device can be used to construct a negative voltage doubler. The output voltage is approximately equal to $-2 \mathrm{~V}_{\text {in }}$ minus the forward voltage drop of each external diode. The performance characteristics for the above converter are shown below. Note that curves A and C show the circuit performance with economical 1N4148 diodes, while curves B and D are with lower loss MBRA120E Schottky diodes.


Figure 31. Doubler Load Regulation, Output Voltage vs. Output Current MAX828


Figure 32. Doubler Load Regulation, Output Voltage vs. Output Current MAX829

## MAX828, MAX829

| Curve | $\mathbf{V}_{\text {in }}(\mathbf{V})$ | Diodes | MAX828 <br> $\mathbf{R}_{\text {out }}(\boldsymbol{\Omega})$ | MAX829 <br> $\mathbf{R}_{\text {out }}(\boldsymbol{\Omega})$ |
| :---: | :---: | :---: | :---: | :---: |
| A | 3.0 | 1 N4148 | 122 | 118 |
| B | 3.0 | MBRA120E | 114 | 106 |
| C | 5.0 | 1N4148 | 96 | 90 |
| D | 5.0 | MBRA120E | 91 | 87 |



Figure 33. Negative Output Voltage Tripler

A single device can be used to construct a negative voltage tripler. The output voltage is approximately equal to $-3 \mathrm{~V}_{\text {in }}$ minus the forward voltage drop of each external diode. The performance characteristics for the above converter are shown below. Note that curves A and C show the circuit performance with economical 1N4148 diodes, while curves B and D are with lower loss MBRA120E Schottky diodes.


Figure 34. Tripler Load Regulation, Output Voltage vs. Output Current MAX828


Figure 35. Tripler Load Regulation, Output Voltage vs. Output Current MAX829

## MAX828, MAX829

| Curve | $\mathbf{V}_{\text {in }}(\mathbf{V})$ | Diodes | MAX828 <br> $\mathbf{R}_{\text {out }}(\boldsymbol{\Omega})$ | MAX829 <br> $\mathbf{R}_{\text {out }}(\boldsymbol{\Omega})$ |
| :---: | :---: | :---: | :---: | :---: |
| A | 3.0 | 1 N4148 | 259 | 246 |
| B | 3.0 | MBRA120E | 251 | 237 |
| C | 5.0 | 1N4148 | 209 | 198 |
| D | 5.0 | MBRA120E | 192 | 185 |



MAX828: Capacitors $=10 \mu \mathrm{~F}$
MAX829: Capacitors $=3.3 \mu \mathrm{~F}$
Figure 36. Positive Output Voltage Doubler

A single device can be used to construct a positive voltage doubler. The output voltage is approximately equal to $2 \mathrm{~V}_{\text {in }}$ minus the forward voltage drop of each external diode. The performance characteristics for the above converter are shown below. Note that curves A and C show the circuit performance with economical 1N4148 diodes, while curves B and D are with lower loss MBRA120E Schottky diodes.


Figure 37. Doubler Load Regulation, Output Voltage vs. Output Current MAX828


Figure 38. Doubler Load Regulation, Output Voltage vs. Output Current MAX829

## MAX828, MAX829

| Curve | $\mathbf{V}_{\text {in }}(\mathbf{V})$ | Diodes | MAX828 <br> $\mathbf{R}_{\text {out }}(\mathbf{\Omega})$ | MAX829 <br> $\mathbf{R}_{\text {out }}(\boldsymbol{\Omega})$ |
| :---: | :---: | :---: | :---: | :---: |
| A | 3.0 | 1 N4148 | 32.5 | 32.2 |
| B | 3.0 | MBRA120E | 27.1 | 25.7 |
| C | 5.0 | 1N4148 | 26.0 | 25.1 |
| D | 5.0 | MBRA120E | 21.2 | 19.0 |



Figure 39. Positive Output Voltage Tripler

A single device can be used to construct a positive voltage tripler. The output voltage is approximately equal to $3 \mathrm{~V}_{\text {in }}$ minus the forward voltage drop of each external diode. The performance characteristics for the above converter are shown below. Note that curves A and C show the circuit performance with economical 1N4148 diodes, while curves B and D are with lower loss MBRA120E Schottky diodes.


Figure 40. Tripler Load Regulation, Output Voltage vs. Output Current MAX828


Figure 41. Tripler Load Regulation, Output Voltage vs. Output Current MAX829

## MAX828, MAX829

| Curve | $\mathbf{V}_{\text {in }}(\mathrm{V})$ | Diodes | MAX828 <br> $\mathbf{R}_{\text {out }}(\boldsymbol{\Omega})$ | MAX829 <br> $\mathbf{R}_{\text {out }}(\boldsymbol{\Omega})$ |
| :---: | :---: | :---: | :---: | :---: |
| A | 3.0 | 1 N4148 | 110 | 111 |
| B | 3.0 | MBRA120E | 96.5 | 96.7 |
| C | 5.0 | 1N4148 | 84.5 | 87.3 |
| D | 5.0 | MBRA120E | 78.2 | 77.1 |



Figure 42. Paralleling Devices for Increased Negative Output Current

An increase in converter output current capability with a reduction in output resistance can be obtained by paralleling two or more devices. The output current capability is approximately equal to the number of devices paralleled. A single shared output capacitor is sufficient for proper operation but each device does require it's own pump capacitor. Note that the output ripple frequency will be complex since the oscillators are not synchronized. The output resistance is approximately equal to the output resistance of one device divided by the total number of devices paralleled. The performance characteristics for a converter consisting of two paralleled devices is shown below.


Figure 43. Parallel Load Regulation, Output Voltage vs. Output Current MAX828


Figure 44. Parallel Load Regulation, Output Voltage vs. Output Current MAX829

## MAX828, MAX829

| Curve | $\mathbf{V}_{\text {in }}(\mathrm{V})$ | $\mathbf{R}_{\text {out }}(\Omega)$ |
| :---: | :---: | :---: |
| A | 5.0 | 13.3 |
| B | 3.0 | 17.3 |
| C | 5.0 | 14.4 |
| D | 3.0 | 17.3 |



Figure 45. External Switch for Increased Negative Output Current

The output current capability of the MAX828 and MAX829 can be extended beyond 600 mA with the addition of two external switch transistors and two Schottky diodes. The output voltage is approximately equal to $-\mathrm{V}_{\mathrm{in}}$ minus the sum of the base emitter drops of both transistors and the forward voltage of both diodes. The performance characteristics for the converter are shown below. Note that the output resistance is reduced to 0.9 and 1.0 ohms for the 828 and 829 respectively.



Figure 48. Positive Output Voltage Doubler with High Current Capability

The MAX828/829 can be configured to produce a positive output voltage doubler with current capability in excess of 500 mA . This is accomplished with the addition of two external switch transistors and two Schottky diodes. The output voltage is approximately equal to $2 \mathrm{~V}_{\text {in }}$ minus the sum of the base emitter drops of both transistors and the forward voltage of both diodes. The performance characteristics for the converter are shown below. Note that the output resistance is reduced to $1.8 \Omega$.


Figure 51. A Positive Doubler, with a Negative Inverter

## MAX828, MAX829

All of the previously shown converter circuits have only single outputs. Applications requiring multiple outputs can be constructed by incorporating combinations of the former circuits. The converter shown above combines Figures 24 and 36 to form a negative output inverter with a positive output doubler. Different combinations of load regulation are shown below. In Figures 52 and 53 the positive doubler has a constant $\mathrm{I}_{\text {out }}=15 \mathrm{~mA}$ while the negative inverter has the variable load. In Figures 54 and 55 the negative inverter has the constant $\mathrm{I}_{\text {out }}=15 \mathrm{~mA}$ and the positive doubler has the variable load.


Figure 52. Negative Inverter Load Regulation, Output Voltage vs. Output Current, MAX828


Figure 54. Positive Doubler Load Regulation, Output Voltage vs. Output Current, MAX828

Figure 53. Negative Inverter Load Regulation, Output Voltage vs. Output Current, MAX829


Figure 55. Positive Doubler Load Regulation, Output Voltage vs. Output Current, MAX829


Inverter Size $=0.5$ in x 0.2 in
Area $=0.10 \mathrm{in}^{2}, 64.5 \mathrm{~mm}^{2}$
Figure 56. Inverter Circuit Board Layout, Top View Copper Side

TSOP-5
CASE 483
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SCALE 2:1
 Mounting Techniques Reference Manual, SOLDERRM/D.

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